## **HyNet North West**

## OUTLINE CONSTRUCTION ENVIRONMENT MANAGEMENT PLAN (OCEMP)

# Appendix 1 Outline Soil Management Plan (Clean)

### **HyNet Carbon Dioxide Pipeline DCO**

Planning Act 2008

The Infrastructure Planning (Applications: Prescribed Forms and Procedure) Regulations 2009 – Regulations 5(2)(a)

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#### 1. INTRODUCTION

#### 1.1. PROJECT BACKGROUND

- 1.1.1. This Outline Soil Management Plan (SMP) supports the assessment contained in Chapter 11 Land and Soil (Volume II) and is an appendix to the Outline Construction Environmental Management Plan (Document reference: D.6.5.4).
- 1.1.2. The Applicant intends to build and operate a new underground carbon dioxide (CO<sub>2</sub>) pipeline from Cheshire, England to Flintshire, Wales with necessary Above Ground Installations (AGIs) and Block Valve Stations (BVSs), hereafter referred to as the 'DCO Proposed Development'. Further details of each element of the DCO Proposed Development are set out in **Chapter 3 Description of the DCO Proposed Development (Volume II).**
- 1.1.3. The DCO Proposed Development will form part of HyNet North West ('the Project'), which is a hydrogen supply and Carbon Capture and Storage ('CCS') project. The goal of the Project is to reduce CO<sub>2</sub> emissions from industry, homes and transport and support economic growth in the North West of England and North Wales. The wider Project is based on the production of low carbon hydrogen from natural gas. It includes the development of a new hydrogen production plant, hydrogen distribution pipelines, hydrogen storage and the creation of CCS infrastructure. CCS prevents CO<sub>2</sub> entering the atmosphere by capturing it, compressing it and transporting it for safe, permanent storage.
- 1.1.4. Further details of each element of the DCO Proposed Development are set out in Chapter 3 Description of the DCO Proposed Development (Volume II).

#### 1.2. SOIL SENSITIVITY

- 1.2.1. Reading Agricultural Consultants (RAC) conducted a detailed Agricultural Land Classification (ALC) survey, between March and May 2022 (Ref. 9). This supplemented existing ALC survey data produced by ADAS (Ref. 1). ALC surveys determine the quality of agricultural land on a 5-point scale, with Grade 1 being excellent quality and grade 5 being very poor-quality (Ref. 6). The grading is based on climatic, site and soil properties.
- 1.2.2. The National Planning and Policy Framework (NPFF) (Ref. 7) and Planning Policy Wales Edition 11 (PPW) (Ref. 8) defines land classified as Grades 1, 2 and 3a as the Best and Most Versatile (BMV) agricultural land. PPW states that BMV land "should be conserved as a finite resource for the future".

- 1.2.3. Non-BMV soil should also be treated as a finite resource as "any loss or degradation of this resource reduces the national stock and the capacity to support ecosystem services in all cases" (Ref. 4).
- 1.2.4. IEMA (2022) **(Ref. 4)** guidance states that "in the first instance, developers should be seeking to avoid negative effects on land and soil... Adapting the generic mitigation hierarchy to soils: avoid > minimise > restore on site > reuse off-site".
- 1.2.5. Without implementing suitable soil handling practices, soils are prone to degradation which leads to numerous environmental impacts both on and offsite, such as:
  - Soil erosion (loss of a resource);
  - Carbon release (disturbance of organic rich soils);
  - Loss of soil organic matter leading to a decline in soil and poor soil structure;
  - Soil compaction leading to loss of soil structure and waterlogging, restricting aeration and rooting potential;
  - Sedimentation of water features, reducing biological productivity and habitat quality;
  - Loss of soil biological activity; and
  - Visual impact of slope failure or soil erosion.

#### 1.3. REPORT PURPOSE AND LIMITATIONS

- 1.3.1. This Outline SMP has been produced to ensure that effects on soil resources are minimised, that adequate provisions for all land being returned to productive agricultural use are made, and to minimise loss of BMV land as a result of the DCO Proposed Development. The Outline SMP provides guidance on appropriate soil management practices (for the categories explained below) and requirements for the development of the Detailed SMP (that will be completed by the appointed Construction Contractor(s)). This Outline SMP:
  - Describes soil handling methods (stripping, stockpiling and reinstatement)
  - Describes required monitoring procedures for soil management during, and after, construction;
  - Describes roles and responsibilities suitable for monitoring soil during the construction phase; and
  - Describes suitable methods for restoration of land to its former use.
- 1.3.2. The following bodies will be consultees on the Detailed SMP and associated Soil Resource Plan:

•	Welsh Government – Soil, Peatland and Agricultural Land Use Planning Unit (LQAS@gov.wales)

#### 2. METHODOLOGY

#### 2.1. SOURCES OF INFORMATION

- 2.1.1. Reading Agricultural Consultants (RAC) conducted detailed ALC surveys, between March and May 2022, that covered the Newbuild Infrastructure Boundary (Ref. 9 & 10). The associated ALC survey reports can be found within Appendix 11.4 Agricultural Land Classification and Soil Resources (Newbuild Carbon Dioxide Pipeline) Report [REP4-132] and Appendix 11.5 Agricultural Land Classification and Soil Resources (Block Valve Stations) Report [REP4-133].
- 2.1.2. This Outline SMP is informed by:
  - Reading Agricultural Consultants (RAC) (2022). HyNet Pipeline Agricultural Land Classification and Soil Resources (Ref. 9).
  - Reading Agricultural Consultants (RAC) (2022). HyNet Pipeline Agricultural Land Classification and Soil Resources - Talacre and Block Valves (Ref.10).

#### 2.2. LIMITATIONS

- 2.2.1. This Outline SMP does not assess potential soil resources in non-agricultural land areas identified by the ALC survey (**Ref. 9**). The appointed Construction Contractor(s) will commission a soil resource survey of these areas, if soil resources are identified. The findings of this will be implemented into the Detailed SMP to ensure appropriate management of non-agricultural soils.
- 2.2.2. Peat areas within the DCO Proposed Development are not covered in this report. These are assessed in the Outline Peat Management Plan (**Document Reference: D.6.5.4.2**).
- 2.2.3. This Outline SMP does not consider human health and controlled water risk assessment associated with potentially contaminated soils. This is discussed in **Chapter 11 Land and Soils [ APP-063]** of the Environmental Statement.
- 2.2.4. During the ALC survey some areas were not surveyed due to access issues. In these instances, the reasonable worst-case scenario has been applied, and these areas have been assumed to be BMV agricultural land. This ensures that necessary provision for soil handling and reinstatement are considered. However, these areas will be surveyed prior to the completion of the Detailed SMP by the appointed Construction Contractor(s) to ensure that the soils present are managed and reinstated appropriately.
- 2.2.5. The soil volume excavation estimations are assumed under a worst-case scenario using the Preliminary Design information that is currently available for the pipeline route, AGIs, BVSs, open-trench and trenchless construction methods. This is to ensure that a suitable estimation of soil and associated

requirements for management have been considered. The reasonable worstcase scenario assumptions used are discussed below.

- 2.2.6. The soil excavation volumes in this Outline SMP do not distinguish between upper and lower subsoil, and basal materials. These distinctions will be made in the detailed Soil Resource Plan (SRP) that will be included in the Detailed SMP.
- 2.2.7. Temporary construction features that require topsoil stripping, have not been considered in the calculations (including temporary access roads, localised and trenchless compounds). These will need to be factored in to soil excavation estimates by the Construction Contractor(s) in the detailed design stage with consideration also given to the use of proprietary systems such as 'trackway' to reduce soil excavation requirements and protect soils in relation to vehicle movements, where engineering and environmental constraints permit.

#### 3. RESULTS

#### 3.1. OVERVIEW

3.1.1. The ALC report for the areas surveyed to date of DCO Proposed Development states that 51% of agricultural land within the Newbuild Infrastructure Boundary is BMV (Ref.9).

#### 3.2. SOIL TEXTURES

- 3.2.1. All soil textures for the sampling points in the ALC survey were determined through hand texturing and confirmed by laboratory analysis where necessary. Soil texture results are displayed in **Annex B** and the laboratory data can be found in the ALC report (**Ref. 9**).
- **3.2.2.** The soil textures determined, and agroclimatic characteristics (see **Annex B**), are used to assign a resilience category for each soil profile that was assessed during the ALC survey. The resilience categories are described in **Table 3.1.**
- 3.2.3. The resilience categories assigned in **Annex B** are limited to the sampling locations assessed during the ALC survey and cannot be generalised across larger areas of the site. To determine the resilience categories, across larger areas, the spatial extent of soil textures, identified by the ALC survey, will be assessed during soil stripping.

Table 3.1 - Soil Resilience Characteristics\*

Topsoil and Subsoil Resilience	Soil Texture, Field Capacity Days and Wetness Class	
Low resilience	Soils with high clay and silt fractions (clays, silty clays, sandy clays, heavy silty clay loams and heavy clay loams) and organo-mineral and peaty soils where the Field Capacity Days (FCD) are 150 or greater.	
	Medium-textured soils (silt loams, medium silty clay loams, medium clay loams and sandy clay loams) where the FCDs are 225 or greater.  All soils in wetness class (WCV or WCVI).	
Madium vaciliana	·	
Medium resilience	Clays, silty clays, sandy clays, heavy silty clay loams, heavy clay loams, silty loams and organo-mineral and peaty soils where the FCDs are fewer than 150.	

Topsoil and Subsoil Resilience	Soil Texture, Field Capacity Days and Wetness Class
	Medium-textured soils (silt loams, medium silty clay loams, medium clay loams and sandy clay loams) where FCDs are fewer than 225.
	Sands, loamy sands, sandy loams and sandy silt loams where the FCDs are 225 or greater or are in wetness classes WCIII and WCIV.
High resilience	Soils with a high sand fraction (sands, loamy sands, sandy loams and sandy silt loams) where the FCDs are fewer than 225 and are in wetness classes WCI to WCII.

<sup>\*</sup>Taken from IEMA (2022). A New Perspective on Land and Soil in Environmental Impact Assessment (Ref. 4).

#### 3.3. SOIL EXCAVATION VOLUME ESTIMATIONS

#### **DESIGN FEATURES**

- 3.3.1. Newbuild Carbon Dioxide Pipeline construction features, that will involve soil excavation, were identified. The dimensions of these features were informed by Chapter 3 Description of the DCO Proposed Development (Volume II) in the Environmental Statement. Where design information is not currently available these are assumed under a reasonable worst-case scenario, to ensure that a suitably robust estimation of soil and associated requirements for soil management have been considered.
- 3.3.2. Dimensions and/or assumptions for the different construction features are as follows:
  - Open trench construction
    - Approximate footprint area along the entire indicative pipeline route used for the EIA: 108,000m<sup>2</sup>; 36,000m x 3m. These are based on assumptions of the final pipeline alignment length, and of the average trench width (considering that usually trenches are trapezoidal in crosssection) and does not consider surface features (e.g., rivers or roads).
    - The depth of the trench will be variable but is anticipated to be within the range of 2.5m 6.0m, with an assumed typical depth of 3m for the purposes of this assessment (Chapter 3 Description of the DCO Proposed Development (Volume II)).
    - Topsoil depth was assumed to be 0.3m.
  - Working width

- Approximate footprint area along the entire indicative pipeline route used for the EIA: 1,044,000m²; 36,000m x 29m (32m working width minus the 3m open trench construction width above).
- Topsoil will be stripped across the full working width.
- Topsoil depth was assumed to be 0.3m.

#### Trenchless crossing pits

- A total of 43 trenchless crossings over the length of the Newbuild Carbon Dioxide Pipeline (Appendix 3.1 – Table of Trenchless Crossings, Volume III) are proposed. An estimated 86 trenchless crossing pits will be required.
- Assumed reasonable worst-case scenario of the most intrusive trenchless crossing method that could be used (Auger Boring method). This is assumed to have an entrance pit footprint area of 32m² (8m × 4m), an exit pit footprint area of 16m² (4m × 4m) and a depth of 9.5m (Chapter 3 Description of the DCO Proposed Development, Volume II).
- Topsoil depth was assumed to be 0.3m.

#### AGIs and BVSs

- There are four AGIs and six BVSs within the Proposed Development.
- Anticipated topsoil and subsoil removal for each, and their associated access roads, has been considered at this design stage and is presented in **Table 3.6**.
- Topsoil depth of 0.3cm is assumed.
- Subsoil excavation is case by case, depending on cut and fill amounts.
- Soil excavation volumes for Stanlow AGI were not calculated as this is a brownfield site.

#### Centralised Compounds

- This Outline SMP has assessed locations for 7 Centralised Compounds within the DCO Proposed Development. Although 7 centralised compounds are being assessed, only 6 are expected to be implemented to facilitate construction of the DCO Proposed Development (Chapter 3 Description of the DCO Proposed Development, Volume II).
- Indicative footprint areas for each Centralised Compound are given in Table 3.5.
- Topsoil will be stripped across the whole area. This is a reasonable worst-case scenario, as it is unlikely that the entire area of all compounds will be stripped. (Chapter 3 Description of the DCO Proposed Development (Volume II)).
- Topsoil and subsoil depths were informed by the average of ALC soil depth data where available. **Table 3.5** shows the soil depths used for the volume calculations.

 There are existing buildings at Wood Farm Compound, therefore, the footprint area reported is the area without buildings, that will need to be stripped (Table 3-5).

#### 3.4. APPROXIMATE EXCAVATION VOLUME ESTIMATES

- 3.4.1. **Table 3.2** indicates that 32,400m³ of topsoil will be excavated for open trench construction (when rounded to the nearest 100m³). The amount of subsoil excavation will depend on the depth of the trench, anticipated to be within the range of 2.5m 6.0m, calculated as a range between 237,600m³ 615,600m³ (respectively). Subsoil excavation volumes are estimated to be 291,600m³ if the typical open trench depth of 3.0m is adhered to.
- 3.4.2. Approximately 313,200m³ of topsoil will be temporarily stripped for the working width **(Table 3.3)**. This topsoil will be reinstated.
- 3.4.3. An estimated 600m³ of topsoil and 19,000m³ of subsoil (when rounded to the nearest 100m³) will be excavated for trenchless pit construction **(Table 3.4).**
- 3.4.4. The volume estimates for open trench and trenchless construction include volumes that are also discussed specifically within the Outline Peat Management Plan (Document Reference Number: D.6.5.4.2).
- 3.4.5. Material from trench excavations will be returned to the trench via backfilling. Any surplus material (that is chemically/physically suitable) shall be beneficially re-used for re-profiling within the working width before topsoil is reinstated on a field-by-field basis.
- 3.4.6. Where surplus soil materials are to be used for re-profiling, impacts on the soil properties (including soil horizon depth and water holding capacity) and ALC grade will be considered. In following pipeline installation best practices and the measures outlined in this Outline SMP, soil re-use will not result in soil degradation or ALC downgrading.
- 3.4.7. Centralised Compounds are anticipated to require approximately 102,700m³ of topsoil to be stripped **(Table 3.5)**. Topsoil will be reinstated at compounds.
- 3.4.8. Approximately 10,762m³ of topsoil and 4,388m³ of subsoil will be excavated for AGI and BVS construction (Table 3.6). Excess subsoil and topsoil will be reused on site where suitable (e.g., for bank or drainage ditch backfilling). The Detailed SMP will detail how bank or drainage ditch backfilling will be undertaken and ensure that this is an appropriate re-use method for the surplus soil material. If there is a requirement for materials to be disposed of off-site, disposal will be undertaken in accordance with waste management regulations (England and Wales). Material will be taken to an offsite recycling facility in accordance with an agreed Materials Management Plan (MMP) produced by the Construction Contractor(s).

**Table 3.2 - Estimated Soil Excavation for Open Trench Construction** 

			Dept	h (m)		Amount of soil stripped (m³)
Design Feature	Number of Features	Area (m²)	Topsoil	Subsoil Upper and lower layers and basal material (if present at given depths)	Tand ayers last at given depths)  Subsoil  Upper and lower layers and basal material (if present at given depths)	
Open Trench Const	ruction					
2.5m trench depth	N/A	108,000	0.3	2.2	32,400	237,600
3.0m trench depth	N/A	108,000	0.3	2.7	32,400	291,600
6.0m trench depth	N/A	108,000	0.3	5.7	32,400	615,600

<sup>\*</sup> Excavation volumes here do not distinguish between upper and lower subsoil layers and basal material. Volumes for each of these will be calculated separately in the detailed SRP that will be produced for the Detailed SMP.

Table 3.3 – Estimated Topsoil Stripping for Working Width

Area (m²)	Topsoil depth (m)	Volume of topsoil stripped (m <sup>3</sup> )
1,044,000m	0.3	313,200

**Table 3.4 - Estimated Soil Excavation for Trenchless Crossings Pits** 

			Depth (m)		Amount of soil stripped (m³)	
Design Feature	Number of Features	Area (m²)	Subsoil  Topsoil  Upper and lower layers and basal material (if present at given depths)		Topsoil	Subsoil Upper and lower layers and basal material (if present at given depths)
Trenchless Cro	ssing Pits					
Entrance Pit	43	32	0.3	9.2	413	12,659
Exit Pit	43	16	0.3	9.2	206	6,330
				Total	619	18,989

<sup>\*</sup> Excavation volumes here do not distinguish between upper and lower subsoil layers and basal material. Volumes for each of these will be calculated separately in the detailed SRP that will be produced for the Detailed SMP.

**Table 3.5 - Estimated Soil Excavation for Centralised Compounds** 

Compound name	Area (m²)	Topsoil depth (m)	Volume of topsoil stripped (m <sup>3</sup> )
Stanlow	66,000	0.32	21,120
Picton Lane	32,000	0.29	9,280
Chorlton Lane	41,000	0.35	14,350
Sealand Road	48,000	0.33	15,840
Wood Farm	55,200	0.30	16,560
River Dee	43,000	0.35	15,050
Northop Hall	35,000	0.30	10,500
		Total	102,700

Table 3.6 - Anticipated Soil Excavation for AGIs and BVSs

Name	Amount of soil stripped (m³)			
	Topsoil	Subsoil Upper and lower layers and basal material (if present at given depths)		
Ince AGI	1,660	0		
Northop Hall AGI	986	567		
Flint AGI	2,850	75		
Rock Bank BVS	700	323		
Mollington BVS	691	107		
Aston Hill BVS	1,025	336		
Cornist Lane BVS	1,090	2,350		
Pentre-Halkyn BVS	770	450		
Babell BVS	990	180		
Total	10,762	4,388		

<sup>\*</sup> Excavation volumes here do not distinguish between upper and lower subsoil layers and basal material. Volumes for each of these will be calculated separately in the detailed SRP that will be produced for the Detailed SMP.

#### 4. SOIL MANAGEMENT DURING CONSTRUCTION

#### 4.1. MAIN PRINCIPLES

- 4.1.1. All soil handling and storage procedures should conform to the Construction Code of Practice for the Sustainable Use of Soils on Construction Sites (Ref. 3). which is referenced in various sections below. Other guidance that is useful for sustainable soil handling is the Good Practice Guide for Handling Soils in Mineral Workings (Ref. 5), British Standard 3882:2015 'Specification for topsoil' (Ref. 12) and A New Perspective on Land and Soil in Environmental Impact Assessment (Ref. 4).
- 4.1.2. The Detailed SMP, that will be produced by the Construction Contractor(s), will include a detailed SRP. This will cover all soil resources for each stage of the DCO Proposed Development and will be in line with the Construction Code of Practice for the Sustainable Use of Soils on Construction Sites (Ref. 3). The SRP will utilise the ALC data to detail soil resources present; provide plans of the soil handling units; soil volumes; location of stockpiles; and restoration criteria.
- 4.1.3. The main threats to soils during construction are trafficking by vehicles/plant, and incorrect handling. These can both cause damage to soil structure through compaction and smearing (deformation). Deformation effects soil functions and the suitability for reuse within the DCO Proposed Development which can increase costs of reinstatement. The risk of deformation increases with increasing field capacity days (FCD) and average annual rainfall (AAR), along with lighter soil textures.
- 4.1.4. The following good practice measures should be followed to minimise the risk of damage to soil structure:
  - A suitably qualified soil scientist will be appointed by the Construction Contractor(s) to monitor all soil handling activities, and good practice measures, as stipulated in this Outline SMP;
  - All individual soil horizons will be stripped, stored, and reinstated separately.
    This includes topsoil, upper and lower subsoil layers, and basal material (if
    present at the stripping depths). These will be identified for the detailed SRP
    in the Detailed SMP, and individually managed;
  - No trafficking of vehicles/plant or materials storage to occur on unprotected topsoil or reinstated soil;
  - Consideration of use of 'trackway' or similar low-ground pressure systems at temporary works zones for vehicles, to reduce excavation and protect soils;

- Only direct movement of soil should occur between the areas being stripped/reinstated to/from designated stockpiles (minimising handling and/or ad hoc storage);
- No soil handling to be carried out when the soil moisture content is above the lower plastic limit.
- No mixing of topsoil with subsoil, or of soil with other materials (unless planned and part of a soil ameliorating strategy);
- Store soil only in designated soil storage areas;
- Stockpiles should not be compacted, but instead gently consolidated;
- Plant and machinery should only work when ground/soil surface conditions enable their maximum operating efficiency and be maintained in a safe and efficient working condition;
- Detailed daily records to be maintained, detailing operations undertaken and Site and soil conditions; and
- Ground should be suitably prepared prior to the reinstatement of soil and an appropriate aftercare plan in place.
- 4.1.5. For each stockpile a plan must be kept and maintained detailing:
  - Material type (topsoil, upper subsoil, lower subsoil) as informed by Annex B;
  - Date/ time when soil was stockpiled and weather conditions;
  - Volume of material;
  - Stockpile location; and
  - Source location of material.
- 4.1.6. The Construction Contractor(s) will be responsible for ensuring that daily records of site and soil conditions are kept, and that a detailed stockpile plan is created and maintained.

#### 4.2. SOIL MOISTURE CONDITIONS FOR HANDLING

- 4.2.1. Handling soils at appropriate moisture levels avoids damage to soil structure (compaction and smearing). Due to the low resilience of the soils within the Newbuild Infrastructure Boundary, adhering to the moisture conditions for handling is extremely important.
- 4.2.2. Following the Institute of Quarrying guidance (Ref. 5), the DCO Proposed Development is based in climatic zone 1. This means that the proposed handling times are between Mid-April and Early-October, when the climatic zone wetness estimates, clay proportion and depth of soil horizon are considered.
- 4.2.3. Removal of excess vegetation, soil stripping, reinstatement and postreinstatement cultivation should not commence if the moisture of the soil (either

in the field or in the stockpiles) is above its lower plastic limit. The plastic limit can be determined using the methodology set out in Supplementary Note 4 'Soil Wetness' in the Institute of Quarrying guidance (Ref. 5).

- 4.2.4. Works can be carried out during occasional showers, however, must cease during prolonged or intense rainfall that increases the soil moisture to above the lower plastic limit. If the works are interrupted by a rainfall event, soil stripping should be suspended; and where the soil profile has already been disturbed, the works should be completed to the base level in that location. Before recommencing work, soil moisture content should be retested.
- 4.2.5. The Construction Contractor(s) should appoint a soil scientist who is suitably experienced and competent in carrying out such soil moisture tests.

#### 4.3. PREPARATORY WORKS

- 4.3.1. Before any work on site involving vehicles commences the Construction Contractor(s) will:
  - Ensure to mark, and signpost the following areas within the Newbuild Infrastructure Boundary including:
    - The undisturbed areas where no construction activities will take place.
       Here soil will not be stripped or trafficked for purposes other than planting, cultivation, and vegetation maintenance;
    - Tree protection zones;
    - Areas from which soils will be stripped;
    - Locations of topsoil and subsoil stockpiles; and
    - Haul routes.
  - Remove scrub vegetation (following any seasonal ecological constraints and mitigation requirements) in the areas requiring stripping; and
  - Remove other vegetation present, so that it is not incorporated into the soil strip. If applicable, cut the grass/crop to ground level.

#### 4.4. STRIPPING

- 4.4.1. The stripping method will follow the method within **Ref. 3** that also includes illustrations of best practice guidance. This method is summarised below.
- 4.4.2. Subsoils will only be stripped if they are being re-used or are of low resilience to reduce compaction. Areas which are going to be used for subsoil storage should have the topsoil stripped to avoid mixing. Subsoils of high to medium resilience do not need stripping underneath haul routes, if they are of low resilience it is advised to strip to a more resilient layer and ensure proper decompaction is carried out following the construction stage.

- 4.4.3. Careful management and consideration of alternative methodologies (e.g. 'trackway') may mean subsoil does not need to be stripped if care is taken.
   Topsoil must be stripped before any subsoil destined for reuse is stripped to reduce the risk of mixing the horizons.
- 4.4.4. Where feasible, vehicles will be tracked to reduce compaction and stripping should be carried out in the driest conditions possible.
- 4.4.5. Key points to minimise soil compaction, and maximise readiness for re-use include:
  - Integrating all soil stripping, moving, storage and reuse/reinstatement operations into the enabling works programme;
  - Ensuring dump trucks only operate on the "basal"/non-soil layer, the wheels must not travel on the soil layer;
  - Ensuring the excavator only operates on topsoil layer;
  - Plant and machinery only working when ground conditions allow maximum efficiency;
  - The moisture content of the soil must be below the lower plastic limit. If it cannot be avoided, provision needs to be made for remediation of soil structure prior or following reinstatement;
  - The operation must cease during periods of rainfall and only recommence if the forecast predicts no further rainfall for a day and soil moisture conditions are suitable:
  - Ensuring the lower soil layers must not be left exposed to rainfall, this is achieved by always stripping to the basal layer before rainfall occurs and/or before stripping is suspended;
  - Protecting the soil and the basal layer from ponding of water by diverting water inflow away from it;
  - Not working when there is standing water on the soil surface or the basal layer;
  - Not mixing topsoil with subsoil and soil with other construction materials; and
  - Storing topsoil on topsoil and subsoil on subsoil or on the basal layer
- 4.4.6. This best practice will be adhered to as far as reasonably practicable.

#### TOPSOIL STRIPPING METHOD

4.4.7. Prior to commencement, the width of each strip will be determined by looking at the length of the excavator less the stand-off to operate. Using the reach of the excavator to its full potential before moving it, reduces the number of areas subject to the weight of the standing plant.

- 4.4.8. Following this, remove surface vegetation by blading off, by scarification and raking (not less than two weeks before stripping commences to reduce the likelihood of anaerobic conditions forming during storage). If the above method is not viable, the careful application of a suitable non-residual herbicide may be necessary.
- 4.4.9. The transport vehicle will run on the basal layer under subsoil if subsoil is also to be stripped. If only topsoil is to be stripped, the vehicle would run on the subsoil layer.
- 4.4.10. Stripping will be undertaken by an excavator standing on the surface of the topsoil, digging the topsoil to its maximum depth (topsoil depths shown in Annex B) and loading into site or off-site transport vehicles.
- 4.4.11. The earthmoving plant used will be appropriate to the volume of soil to be stripped, site size and hauling distances. This will be determined by the Construction Contractor(s) for the Detailed SMP.

#### SUBSOIL STRIPPING METHOD

- 4.4.12. For each soil unit the soil layers above the base/formation layer will be removed in sequential strips that can be up to 6m wide (the reach of a 360° excavator). Using an excavator bucket with teeth is preferable to achieve desired outcome.
- 4.4.13. Where there is a cover of topsoil, that layer is removed first before stripping subsoil to the specified depth.
- 4.4.14. The soil transport vehicle will run on the layer beneath the required subsoil stripping depth.
- 4.4.15. The earthmoving plant used will be appropriate to the volume of soil to be stripped, site size and hauling distances. This will be determined by the Construction Contractor(s) for the Detailed SMP.

#### 4.5. SOIL STORAGE

- 4.5.1. Resilience has been assigned to each soil horizon to inform the height at which soil (**Annex B**) will be stockpiled to. This area has a relatively average AAR (678mm to 792mm) and FCD (152 to 188) which influences the handling resilience of the soil, **Annex A** shows the agroclimatic data by ALC sample point. Stockpile height should not exceed 2m as far as reasonably practicable.
- 4.5.2. Soil stockpiles will be split into different soil types, including topsoil, upper subsoil, lower subsoil, and basal material. Through appropriate separation and storage of soils, particularly for topsoil, this will ensure retention of any associated seed bank within the soils, which will be reinstated in the correct layering post construction.

- 4.5.3. After being stripped, soil units will be stored in stockpiles close to their source and stockpiles should be in areas where they will not be disturbed during construction activities.
- 4.5.4. Soil stripping, storage and reinstatement must be integrated into the enabling works programme by the Construction Contractor(s).

#### 4.6. STOCKPILE LOCATIONS

- 4.6.1. Stockpiles will be located on medium or high resilience soils away from ditches or watercourses to reduce the impact on controlled waters. This will include temporary storage of materials at a minimum distance of 10m from any watercourses and 50m from any watercourse identified on Ordnance Survey 50,000 scale mapping (Ref. 2).
- 4.6.2. Stockpiles will be located away from trees, hedge lines and existing/future excavations. This avoids repeated handling/transfer of soil, reducing potential for degradation of the soil structure.
- 4.6.3. Each source area will have its own stockpile location, with topsoils and subsoils stockpiled separately.
- 4.6.4. Stockpile locations within will be determined by the Construction Contractor(s) when the design has been finalised. The locations will be detailed in the Detailed SMP.

#### 4.7. FORMING THE STOCKPILES

- 4.7.1. Dimensions of the stockpiles may be adjusted but the angle of repose shall not exceed 1 in 2 (25°) even if seeded and regularly maintained.
- 4.7.2. Each stockpile must be clearly marked and labelled with the source area, material type and volume. These labels will be kept up to date.
- 4.7.3. Soil stockpiles should also be clearly mapped.
- 4.7.4. The dry and wet stockpiling methods from **Ref. 3** are summarised below:

#### DRY SOIL STOCKPILING METHOD

- Loose tip heaps of soil from a dump truck starting at the furthest point in the storage area, working towards the access point;
- A tracked excavator or dozer then levels the heaps and firms the surface to enable a second layer to be added;
- Repeat until the stockpile has reached the desired height; and
- With a tracked excavator or dozer, compact and re-grade the sides and top
  of the stockpile to a smooth gradient to reduce infiltration and the likelihood
  of ponding.

#### WET SOIL STOCKPILING METHOD

- Tip soil into a line of heaps to form a "windrow", start at the furthest point, finish at the access point;
- Space windrows sufficiently apart so a tracked dozer or excavator can move between them to heap the soil up to 2m maximum;
- No machinery should traverse the windrow to avoid compaction and subsequent structural damage to the soil;
- Once the soil has reached a non-plastic consistency, which often takes many weeks, combine the windrows to form larger stockpiles using a tracked excavator; and
- Regrade and compact the sides and top of the stockpile using a tracked excavator or dozer, to prevent ponding and infiltration.

#### 4.8. MAINTENANCE OF STOCKPILES DURING STORAGE

4.8.1. Seeding is advised if soils are to be stockpiled for over six months or over winter. In these events stockpiles will be seeded with a suitable grass mix to protect against soil erosion, minimise nutrient loss and maintain its biological activity. The grass will be cut two to three times a year and removed completely before reinstatement of soil.

#### 5. SOIL REINSTATEMENT

#### 5.1. GENERAL METHODS TO BE USED WITHIN RESTORATION

- 5.1.1. All methods should align with the guidance on handling and soil moisture content that have been discussed in this Outline SMP.
- 5.1.2. Any decompaction or remediation activities will be undertaken when the soils are in a suitably dry condition. Soil moisture should be tested using the method outlined in section 4.2.
- 5.1.3. Soil horizons should be reinstated sequentially in the order they were removed basal material, lower subsoil horizons, to upper subsoil horizons, to topsoil. This will be ensured by following best practice for stockpiling which includes clear labelling of stockpiles and soil textures, avoiding horizons being mixed.

#### 5.2. EXCAVATION OF SOIL STOCKPILES

- 5.2.1. The method to be followed for the excavation of soil stockpiles is taken from **Ref. 3** and explained below.
- 5.2.2. Dump trucks will enter on the basal layer (if topsoil and subsoil are stripped) or subsoil (if topsoil only stripped). If a back-acting excavator is used, it must stand on top of the stockpile to load the dump truck. The stockpile will be dug to the base before moving progressively back along its axis.
- 5.2.3. If a front-loading machine is used, any exposed edges or surface of the stockpile will be shaped to reduce the pooling of water at the onset of rain and end of each day.

#### 5.3. PREPARATION OF THE BASE LAYER

- 5.3.1. Areas where stockpiles, haul routes and other high traffic are located will require decompaction before topsoil reinstatement. This includes ripping subsoils in agricultural areas to return them to their ALC grade and not introduce a wetness limitation. For decompaction, a wing-tine ripper is recommended.
- 5.3.2. Large stones and debris should be removed from the area before reinstatement.

#### 5.4. SOIL REINSTATEMENT

- 5.4.1. All horizons will be reinstated in the same order as they were before disturbance, avoiding mixing of textures where possible.
- 5.4.2. Reinstatement will take place when the soil is below the plastic limit, if it rains more than 10mm in 24 hours it is advised to suspend reinstatement until the soil

is below the plastic limit. Soil is not advised to be reinstated when the ground is frozen or in other adverse weather conditions.

- 5.4.3. To return soils to an area the loose tipping method is recommended as this allows minimal disturbance to the soils structure. This method is described below (Ref.3).
- 5.4.4. Loosen the receiving group using a wing-tine ripper, with a toothed bucket (which avoids excessive smearing) and load the stockpiled soil in to dump trucks to transport and discharge the soil into the desired location.
- 5.4.5. The soil will be reinstated in strips based on the reach of the excavator. An excavator will be used to spread the soil to the desired thickness. If replacing both subsoil and topsoil, all subsoil will be laid then all topsoil. Topsoil will be laid without the excavator travelling on the newly placed subsoil.
- 5.4.6. Agricultural topsoil can be mounded to a maximum of 400mm above previous ground level, providing the landowner/farmer is in agreement and the soil meets suitability criteria for reuse. Locally excavated soil material may also be spread across the working width where appropriate to do so.
- 5.4.7. All reinstated topsoil will be cultivated to its full depth to reduce compaction and increase aeration. Cultivation should remove the presence of any large, compacted lumps. For seeding, a maximum aggregate size of 10mm is recommended. If any undesirable materials (such as stones or fill over 50mm in any dimension) are present, it is recommended to remove them by raking or picking.
- 5.4.8. All land will be reinstated to the standards of the baseline ALC grade (prior to disturbance) as far as is reasonably practicable. The limiting factors of each grade can be found in the MAFF revised guidelines and criteria for grading the quality of agricultural land (Ref. 6). This includes all BMV land being returned to its original quality.
- 5.4.9. A target specification for the restored soils (according to location, soil types, end use and required ALC grade) will be developed, by a suitably qualified Soil Scientist, and reported in the Detailed SMP.

#### 6. AFTERCARE OF REINSTATED SOILS

- 6.1.1. After reinstatement, soils tend to self-compact and settle, especially those with low resilience. It can take between one to three years for their structures to stabilise. This can lead to waterlogging and anaerobic conditions, which can contribute to erosion and flooding, but can also lead to negative impacts on root function and plant health.
- 6.1.2. To avoid the negative impacts above reinstatement will be inspected by a competent soil scientist and an aftercare plan developed to help the successful reinstatement of the soils. For example, keeping livestock off reinstated grassland in the winter will reduce the likelihood of compaction due to the soils structure being unstable. The aftercare plan will be prepared by the Construction Contractor as part of the Detailed SMP.

#### 7. SOIL REUSE AND DISPOSAL

- 7.1.1. In the event that there is a soil surplus from construction activities, all suitable (chemically/physically suitable and asbestos free) material will be beneficially reused on site through measures put in place through the Materials Management Plan (MMP) that will be produced by the Construction Contractor(s) as part of the CEMP.
- 7.1.2. If excavated materials are unsuitable for reuse, such as contaminated soils or hazardous materials (not soils i.e., anthropogenic material) this will be removed off-site and disposed in accordance with an agreed MMP. The Construction Contractor(s) will follow appropriate legislative requirements and best practice. The material would be appropriately classified prior to transport to a suitably licenced landfill /treatment centre.
- 7.1.3. The landowner / occupier will be engaged where any off-site disposal is required. In such instances, disposal will be undertaken in accordance with waste management regulations (England and Wales). Further detail is provided in Chapter 14 Materials and Waste (Volume II).

#### 8. SUMMARY AND CONCLUSIONS

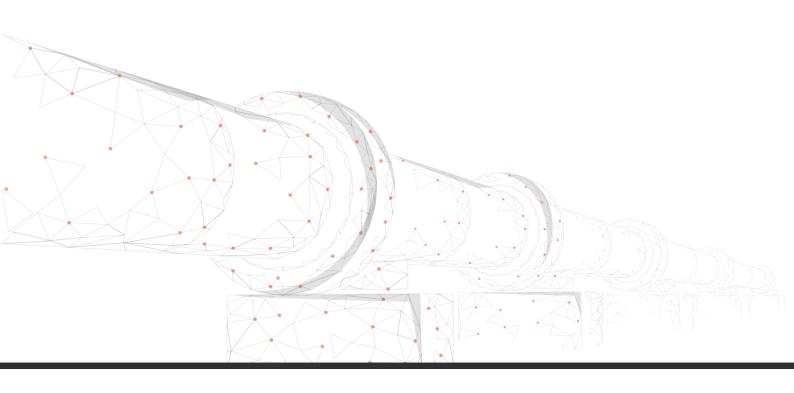
- 8.1.1. This Outline SMP estimates reasonable worst-case volumes of soil excavation and sets out best practice measures for soil management. This best practice will be adhered to during, and after, the construction of the DCO Proposed Development. The Outline SMP also identifies further actions required by the appointed Construction Contractor(s), for the Detailed SMP. It is recognised that there is a degree of professional judgement involved in quantifying assumptions.
- 8.1.2. There are a number of opportunities to reduce the extent of excavation and/or increase the extent of re-use opportunities as good practice measures. These include:
  - reducing excavation depth required for the DCO Proposed Development infrastructure;
    - Seeking to minimise open trench depth towards the lower end of the range.
    - avoiding wholescale excavation of subsoil at AGIs and BVSs.
  - consideration of application of 'trackway' to reduce excavation volumes and protect soil at relevant locations where vehicle movements are required in temporary works zones;
  - re-use of all excavated material for engineering fill and landscaping; and
  - appropriate re-use of excavated material for reinstatement and profiling on site.
- 8.1.3. Applying the reasonable assumptions discussed above, it is expected there will be sufficient re-use opportunities within the Newbuild Infrastructure Boundary to avoid any surplus.
- 8.1.4. Any material identified as waste shall be managed in accordance with appropriate legislation and regulatory guidance.

#### 3. REFERENCES

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- Ref. 12 British Standard (BS) 3882:2015 'Specification for topsoil'

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## Annexures



## Annex A

### **AGROCLIMATIC DATA**

Table A1 - Agroclimatic data by ALC sample point

ALC sample points	Field Capacity Days	Average Annual Rainfall
1 to 52	155	691
53 to 94	152	678
95 to 137	156	
138 to 188	158	
192 to195	171	
196 to 215	180	778
238 to 269	184	792
270 to 294	188	

## Annex B

### **SOIL RESILIENCE**

Table B1 - Soil textures and their accronyms

Soil texture	
cS	coarse sand
mS	medium sand
fS	fine sand
LcS	loamy coarse sand
LmS	loamy medium sand
LfS	loamy fine sand
cSL	coarse sandy loam
mSL	medium sandy loam
fSL	fine sandy loam
cSZL	coarse sandy silt loam
mSZL	medium sandy silt loam
fSZL	fine sandy silt loam
MZ	marine light silt
ZL	silt loam
cSCL	coarse sandy clay loam
SCL	sandy clay loam
fSCL	fine sandy clay loam
mCL	medium clay loam
CL	clay loam (borderline)
hCL	heavy clay loam
mZCL	medium silty clay loam
ZCL	silty clay loam (borderline)
hZCL	heavy silty clay loam
SC	sandy clay
LC	loamy clay
С	clay
ZC	silty clay

Sample number	Topsoil (T)	Depth	of horizon	Soil texture	Resillience
1	Т	0	21	hZCL	Low
		21	35		Medium
		35 80			Medium Low
2	Т	0			Low
	Т	10	25	С	Low
		25			Low
		50 75			Low
3	Т	0	20		Low Low
pit	ı	20			Low
		60	120	PL	Low
4	Т	0			Low
	Т	5 25			Low
		33			Low Low
		70		С	Low
5	Т	0	25	С	Low
		25			Low
	-	48			Low Low
6	Т	25			Low
		45			Low
		80	120	PL	Low
7	Т	0	22		Low
		22			Low
		55 80			Low Low
8	Т	0		-	Medium
		39	50	SCL	Medium
		50			Low
	_	80			Low Medium
9	Т	36			Medium
		70			Low
		100			Low
10	Т	0			Medium
		35 48			Medium Low
		90			Low
11	Т	0	35	SCL	Medium
		35			Low
		39 50			Medium Low
		90			Low
12	Т	0	35	SCL	Medium
		35			Medium
		40			Medium
		93 95			Low Low
13	Т	0			High
		35			Medium
ĺ		40			Low
		50 90			Low High
ĺ		100			High
14	Т	0	30		Medium
ĺ		30			Medium
ĺ		75 80			Medium Low
15	Т	0	38		Medium
	'	38			Medium
		48			Low
ĺ		70			Low
16	<b>-</b>	90			Low Medium
16	Т	35			Medium
		55			Low
		80			Low
17	Т	0	38		Medium
ĺ		38 48			Low Low
I		.0	<u>50</u>	-	

18	I		90	120	С	Low
19	18	Т	0	38	mCL	
19						
19						
	19	Т				Medium
Section   Sect						
20						
Pit						
100		Т				
21	ρit					
Second   S						
See	21	Т				
22			68	90	С	
1	22	Т				
Pit						Low
Pit		_				
A0		T				
24						
24						
Section   Sect	24	Т				
25						
36	25	т				
26	23	,				
26						
36	26	Т				
120   C   Low	20	·				
27 T O S SCL Medium  42 TO C Low  42 TO C Low  50 120 C Low  28 T O 25 TSZL High  43 90 C Low  44 SCL Medium  45 SCL Medium  46 SCL Medium  47 SCL SCL Medium  48 SCL Medium  48 SCL Medium  48 SCL Low  48 SCL Medium  48 SCL Medium  48 SCL Low  48 SCL Medium  48 SCL Low  49 SCL Medium  40 90 C Low  40 SCL Medium  40 SCL Low  40 SCL Medium						
35	27	Т				
T						Medium
120   C   Low						
25						
35	28	Т				
143						
29 T 0 38 mCL Medium  58 90 C Low  90 120 C Low  30 T 0 35 mCL Medium  45 100 C Low  100 120 C Low  31 T 0 20 mCL Medium  45 100 C Low  100 120 C Low  31 T 0 20 mCL Medium  45 100 C Low  100 120 C Low  45 38 70 C Low  46 Medium  47 20 35 mCL Medium  48 70 C Low  48 70 90 C Low  100 120 C Low  100 C				90	С	
38		_				
Second   S	29	Т				
T						Low
35	20	<b>-</b>				
100	30	'				
T						
20   35   mCL   Medium	31	Т				
38		·	20	35	mCL	Medium
T   O   32   SCL   Medium						
120   C   Low						
32 45 SL High 45 51 mCL Medium 51 80 C Low 80 100 C Low 100 120 C Low  100 33 mszL High 33 40 SCL Medium 40 90 C Low 90 120 C Low						Low
45   51   mCL   Medium     51   80   C   Low     80   100   C   Low     100   120   C   Low     100   33   mszL   High     33   40   SCL   Medium     40   90   C   Low     90   120   C   Low	32	Т				
51						
100     120     C     Low       33     T     0     33     mSZL     High       33     40     SCL     Medium       40     90     C     Low       90     120     C     Low						Low
33 T 0 33 mszL High 33 40 SCL Medium 40 90 C Low 90 120 C Low						
40 <u>90</u> C <b>Low</b> 90 120 C <b>Low</b>	33	Т	0		mSZL	High
90 120 C Low						
	34	Т	0	40	mSZL	

-				•	
		40			Medium
		48 100			Low Low
35	Т	0	40	mSL	High
		40	<u>100</u>	fS	High
		100			High
36	Т	0 40	40 43	mSZL SCL	High Medium
		43			Low
		90		С	Low
37	Т	0	43	mSZL	High
		43			Medium
		60 100		C C	Low Low
38	Т	0	38		High
	·	38		С	Low
		70			Low
		100		С	Low
39	Т	0 40	40		High
		60	<u>60</u> 120	C	Medium Low
40	Т	0	40	mSZL	High
		40	55	SCL	Medium
		55		С	Low
		70 80		C C	Low
41	Т	0	40		Low Medium
71	'	40	50		Medium
		50	<u>100</u>	mS	High
		100	120	mS	High
42	Т	0	38		Medium
		38 70			Medium Low
		90			Low
43	Т	0	28	SCL	Medium
		28			Medium
		46			Low
		85 <u>100</u>		C C	Low Low
44	Т	0	27	SCL	Medium
		27	45	SCL	Medium
		45			High
		78 <u>105</u>			Low Low
45	Т	0	27	mCL	Medium
		27	40	mCL	Medium
		40			Medium
		74			Low
		85 <u>100</u>	100 120		Low Low
46	Т	0	27	SCL	Medium
		27	40		High
		40			High
		75 105		hCL C	Low Low
47	Т	0	27	SCL	Medium
-71	, i	27	45		Medium
		45			Low
		70			Medium
48	Т	0 27	27 45	SCL SCL	Medium Medium
		45		SCL	Low
		65			Low
		<u>100</u>			Low
49	Т	0		SCL	Medium
		27	45 95	SC C	Low
		45 <u>95</u>			Low Low
50	Т	0	29	SL	High
		29	51	SL/SCL	Medium
		51			Low
		60 80		C C	Low
		50	120	Ŭ	Low

51	Т	0	28	SL	High
		28	40		Medium
		40	50		Low
		50	80		Low
		80	120	С	Low
52	Т	0	28	SL	High
		28	40	SL/SCL	Medium
		40	55	С	Low
		55	65	SL	High
		65	95	С	Low
		<u>95</u>	120	С	Low
53	Т	0	28	oSCL SCL	Low
		28 43	43 55	hCL	Medium
		43 55	55 75	C	Low
		75		C	Low Low
54	Т	0	36	SL	High
54	'	36	70	LS	High
		70	120	LS	High
55	Т	0	35	SL	High
33	'	35	70		High
		70	120	LS	High
56	Т	0	28	SCL	Medium
30	'	28	40		High
		40	80	SL	High
		80	120	CL/C	Low
57	Т	0	28	SL	High
0.	,	28	45	SL	High
		45	120	oLS	Low
58	Т	0	38	SL	High
		38	70	SL	High
		70	105	mS	High
		<u>105</u>	120	mS	High
59	Т	0	38	SL	High
		38	70	SL	High
		70	110	LS	High
		<u>110</u>	120	mS	High
60	Т	0	38	SL	High
		38	80		High
		80	105		Low
		105	120	LS	High
61	Т	0	40	SL	High
		40	65	SL	High
		65	95		High
1			120	SCI	Madium
	_	95	120		Medium
62	Т	95	30	ohZCL	Low
		95 0 29	30 120	ohZCL PL	Low Low
62	Т	95 0 29 0	30 120 10	ohZCL PL PL	Low Low Low
		95 0 29 0 10	30 120 10 23	ohZCL PL PL ohZCL	Low Low Low Low
	Т	95 0 29 0	30 120 10	ohZCL PL PL ohZCL	Low Low Low Low Low
63	T T	95 0 29 0 10 23 40	30 120 10 23 40 120	ohZCL PL PL ohZCL PL PL	Low Low Low Low Low Low
	Т	95 0 29 0 10 23	30 120 10 23 40	ohZCL PL PL ohZCL PL	Low Low Low Low Low Low
63	T T	95 0 29 0 10 23 40	30 120 10 23 40 120	ohZCL PL ohZCL PL PL ohZCL	Low Low Low Low Low Low Low Low
63	T T	95 0 29 0 10 23 40 0 29	30 120 10 23 40 120 30	ohZCL PL OhZCL PL PL OhZCL PL	Low Low Low Low Low Low
63	T T	95 0 29 0 10 23 40 0 29	30 120 10 23 40 120 30 120	ohZCL PL ohZCL PL ohZCL PL ohZCL PL	Low Low Low Low Low Low Low Low Low
63 64 65	T T	95 0 29 0 10 23 40 0 29	30 120 10 23 40 120 30 120 29	ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL OhZCL OhZCL	Low
63 64 65	T T	95 0 29 0 10 23 40 0 29 0 29	30 120 10 23 40 120 30 120 29 120 28 35	ohZCL PL OhZCL PL OhZCL PL OhZCL PL OhZCL PL OhZCL PL	Low
63 64 65	T T	95 0 29 0 10 23 40 0 29 0 29	30 120 10 23 40 120 30 120 29 120 28 35	ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL	Low
63 64 65 66	T T T	95 0 29 0 10 23 40 0 29 0 29 0 28 35	30 120 10 23 40 120 30 120 29 120 28 35 120	ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL OhZCL OhZCL OhZCL OhZCL OhZCL OhZCL OhZCL OhZCL	Low
63 64 65 66	T T T	95 0 29 0 10 23 40 0 29 0 28 35	30 120 10 23 40 120 30 120 29 120 28 35 120 28	ohZCL PL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL chZCL CL/C	Low
63 64 65 66	T T T	95 0 29 0 10 23 40 0 29 0 29 0 28 35	30 120 10 23 40 120 30 120 29 120 28 35 120 28	ohZCL PL	Low
63 64 65 66	T T T	95 0 29 0 10 23 40 0 29 0 28 35 0 28 40	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75	ohZCL PL	Low
63 64 65 66	T T T	95 0 29 0 10 23 40 0 29 0 28 35 0 28 40 75	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120	ohZCL PL pL	Low
63 64 65 66	T T T	95 0 29 0 10 23 40 0 29 0 28 35 0 28 40 75	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120	ohZCL PL pL	Low
63 64 65 66	T T T	95 0 29 0 10 23 40 0 29 0 28 35 0 28 40 75	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120	ohZCL PL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL ohZCL PL pL oCL CL/C PL hZCL PL pL	Low
63 64 65 66 67	T T T	95 0 29 0 10 23 40 0 29 0 29 0 28 35 0 28 40 75 0 25 40 0 15	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120 25 40 120	ohZCL PL oCL CL/C PL hZCL ohZCL PL ohZCL C	Low
63 64 65 66 67	T T T	95 0 29 0 10 23 40 0 29 0 28 35 0 28 40 75 0 25 40	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120 25 40 120	ohZCL PL oCL CL/C PL hZCL ohZCL PL ohZCL C	Low
63 64 65 66 67	T T T	95 0 29 0 10 23 40 0 29 0 29 0 28 35 0 28 40 75 0 25 40 0 15	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120 25 40 120	ohZCL PL OhZCL CL/C PL AZCL OhZCL CL/C PL SCL	Low
63 64 65 66 67 68	T T T T	95 0 29 0 10 23 40 0 29 0 29 0 28 35 0 28 40 75 0 25 40 0 15 28 0 28	30 120 10 23 40 120 30 120 28 35 120 28 40 75 120 25 40 120	ohZCL PL OhZCL PL OhZCL PL OhZCL PL OhZCL PL OhZCL PL OCL CL/C PL hZCL OhZCL PL SCL SCL	Low
63 64 65 66 67 68	T T T T	95 0 29 0 10 23 40 0 29 0 28 35 0 28 40 75 0 25 40 0 15 28 40 28 40 40	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120 25 40 120 25 40 120	ohZCL PL sCL CL/C PL hZCL OhZCL CL/C SCL SCL SCL	Low
63 64 65 66 67 68	T T T T	95 0 29 0 10 23 40 0 29 0 29 0 28 35 0 28 40 75 0 25 40 0 15 28 0 28 40 68	30 120 10 23 40 120 30 120 28 35 120 28 40 75 120 25 40 120 25 40 120 28 40 120	ohZCL PL sCL/C PL hZCL OhZCL PL sCL C C C C	Low
63 64 65 66 67 68	T T T T	95 0 29 0 10 23 40 0 29 0 28 35 0 28 40 75 0 25 40 0 15 28 40 28 40 40	30 120 10 23 40 120 30 120 29 120 28 35 120 28 40 75 120 25 40 120 25 40 120	ohZCL PL sCL CL/C PL hZCL OhZCL CL/C SCL SCL SCL	Low

71	Т	0	28	SCL	Medium
		28	40	SCL	Medium
		40	65	SCL	Medium
		65	80	С	Low
		<u>80</u>	120	С	Low
95	Т	0	30	mSZL	High
		30	40	mSZL	High
		40	68	SCL	Medium
		68	<u>85</u>	С	Low
		85	120	С	Low
96	Т	0	39	mZCL	Medium
		39	<u>60</u>	hCL	Low
		60	120	С	Low
97	Т	0	33	mCL	Medium
		33	<u>60</u>	С	Low
		60	120	С	Low
98	Т	0	20	mCL	Medium
		20	33	hCL	Low
		33	<u>60</u>	С	Low
		60	120	С	Low
99	Т	0	38	SCL	Medium
		38	55	SCL	Medium
		55	80	С	Low
		80	120	С	Low
100	Т	0	33	hCL	Low
	•	33	<u>50</u>	С	Low
		50			Low
101	Т	0	40	mCL	Medium
	·	40	55		Low
		55	80		Low
		80			Low
102	Т	0	35	mCL	Medium
102	'	35			Low
		45			Low
		90			Low
103	Т	0	30		Medium
103	'	30	40		Medium
		40			Medium
		50			Low
104	Т	0			Low
104	'	35			Low
		90			Low
105	Т	0			Medium
103	1	35			Medium
		68			Low
		80			Low
106	Т	0	25		Medium
106	ı	25			Low
		28			Low
407	_	0			Medium
107	Т	36			
		48			Low Low
		70			Low
108	<b>T</b>	0	35		High
108	Т	35			Medium
		43			Low
		80			Low
109	Т	0	30		Medium
109	'	30			Medium
		40			Low
		55			Low
		85			Low
110	Т	0	35		Medium
110	· '	35			Low
		40			
		58			Low Low
		90			
444	-	0			Low
111	Т	30			Low
		42			Low
		- 4/	<u>80</u>	Ü	Low
			120	С	LOW
440	-	90			Low
112	Т		20	mZCL	Low Medium Medium

113						
113						
113						
114	113	т				
114						
114			40	70	SCL	Medium
114						
115						
115	114	Т				
115						
115			48	75	С	
115						
116						
116	115	Т				
116						
118						
118	116	Т	0	30	mCL	Medium
118			30			
118						
118						
119	118	Т				
119		· .				
119 T 0 35 hCL						
120						
120	119	Т				
120						
120						
121			90	120	С	
121	120	Т	0	38	SCL	Medium
121						
121						
121						
122	121	Т				
122			30	40	mCL	
122						
122 T 0 35 mSZL High Medium 48 70 C Low 123 T 0 30 SCL Medium 43 90 C Low 124 T 0 20 SCL Medium 43 90 C Low 124 T 0 20 SCL Medium 48 70 C Low 124 T 0 20 SCL Medium 48 70 C Low 126 Medium 48 70 C Low 70 80 SCL Medium 48 70 C Low 70 80 SCL Medium 48 70 C Low 70 80 SCL Medium 125 T 0 20 mCL Medium 120 ms High 121 ms High 122 ms High 125 T 0 20 mCL Medium 126 T 0 33 hCL Low 127 T 0 33 hCL Low 128 T 0 33 hCL Low 129 C Low 120 C Low 120 C Low 121 C Low 122 C Low 123 S CL Medium 124 C Low 125 C Low 126 C Low 127 C Low 128 C Low 129 C Low 120 C Low						
123 T 0 30 SCL Medium  124 T 0 20 SCL Medium  124 T 0 20 SCL Medium  125 T 0 20 SCL Medium  126 T 0 20 SCL Medium  127 T 0 20 SCL Medium  128 T 0 30 Medium  129 C Low  120 C Low  120 C Low  120 SCL Medium  120 SCL Medium	122	т				
123	122	'				
123 T 0 30 SCL Medium  130 43 SCL Medium  143 90 C Low  124 T 0 20 SCL Medium  125 T 0 20 Medium  126 T 0 20 Medium  127 T 0 30 Medium  128 T 0 30 Medium  130 Medium  148 70 C Low  160 Medium  170 Medium  180 Medium  190 Medium  Medium  Medium  Medium  Medium  Medium  120 C Low			48	<u>70</u>	С	
124						
124	123	Т				
124						
124						
125	124	Т	0	20	SCL	
125			20	35		Medium
T						
125						
125       T       0       20       mS       High         126       T       0       20       mCL       Medium         126       T       0       33       hCL       Low         127       T       0       33       hCL       Low         127       T       0       30       hCL       Low         127       T       0       30       hCL       Low         128       T       0       33       hCL       Low         129       C       Low       Low       Low       Low         120       C       Low						
125       T       0       20       mCL       Medium         20       38       70       C       Low         126       T       0       33       hCL       Low         127       T       0       33       hCL       Low         127       T       0       30       hCL       Low         127       T       0       30       hCL       Low         128       T       0       33       hCL       Low         129       C       Low       Low       Low       Low         120       C       Low						
126	125	Т	0	20	mCL	
126       T       0       33       hCL       Low         33       38       hCL       Low         40       60       C       Low         50       120       C       Low         127       T       0       30       hCL       Low         50       120       C       Low         128       T       0       33       hCL       Low         33       38       hCL       Low         38       60       C       Low         Low       Low       Low         Low						Medium
126 T 0 33 hCL LOW						
127 T 0 30 hCL LOW 120 C LOW 127 T 0 30 hCL LOW 128 T 0 33 hCL LOW 128 T 0 33 hCL LOW 139 50 hCL LOW 140 C LOW 150 120 C LOW 150 LOW	400					
127 T 0 30 hCL Low 128 T 0 33 hCL Low 128 T 0 33 hCL Low 139 50 hCL Low 120 C Low 140 Low 150 120 C Low 140 Low 150 33 hCL Low 150 C Low	126	T				
127 T 0 30 hCL LOW 128 T 0 33 hCL LOW 128 T 0 33 hCL LOW 139 50 hCL LOW 140 C LOW 150 120 C LOW 150 33 hCL LOW 150 120 C LOW 160 120 C LOW 160 LOW 170 C LOW 180 LOW						
128 T 0 33 hCL Low 139 hCL Low 140 C Low 150 120 C Low						
128       T       0       33       hCL       Low         33       38       hCL       Low         4       38       60       C       Low         60       120       C       Low	127	Т				
128 T 0 33 hCL Low Low 38 hCL Low Low 60 120 C Low						
33 38 hCL Low 38 60 C Low 60 120 C Low	420	<b>-</b>				
38 <u>60</u> C <b>Low</b> 60 120 C <b>Low</b>	128	Т				
60 120 C <b>Low</b>						
T 0 30 mSZL High			60	120	С	
	129	Т	0	30	mSZL	High

		30	40	mSZL	High
		40	49	SCL	Medium
		49	75	С	Low
		75 80	<u>80</u> 120	C C	Low
400	_		38	ZL	Low
138	Т	0 38	55	ZL ZL	Medium Medium
		55	<u>100</u>	fSL	High
		100	120	fSL	High
139	Т	0	43	LfS	High
		43	<u>70</u>	fS	High
		70	120	fS	High
140	Т	0	35	ZL	Medium
		33	43	fSL	High
		43	<u>80</u>	fS	High
		80	120	fS	High
141	Т	0 45	45 <u>80</u>	fSL fS	High
		80	120	fS	High High
142	Т	0	43	LfS	High
142	'	43	80	fS	High
		80	120	fS	High
143	Т	0	43	fSL	High
		43	<u>80</u>	fS	High
		80	120	fS	High
144	Т	0	39	ZL	Medium
		39	<u>80</u>	fS	High
		80	120	fS	High
145	Т	0	30	ZL ZL	Medium
		30 43	43 <u>80</u>	ZL fS	Medium High
		80	120	fS	High
146	Т	0	30	ZL	Medium
		30	43	ZL	Medium
		43	<u>80</u>	fS	High
		80	120	fS	High
147	Т	0	40	fSL	High
		38	58	fS	High
		58 70	<u>70</u> 120	fS fS	High
148	Т	0	30	ZL	High Medium
140	'	30	43	ZL	Medium
		43	<u>100</u>	fS	High
		100	120	fS	High
149	Т	0	30	ZL	Medium
		30	43	ZL	Medium
		43	<u>100</u>	fS	High
450	_	100 0	120 30	fS mZCL	High
150	Т	30	43	mZCL	Medium Medium
		43	<u>100</u>	fS	High
		100	120	fS	High
151	Т	0	30	ZL	Medium
		30	48	ZL	Medium
		48	<u>100</u>	ZL	Medium
		100	120	fS	High
152	Т	0	30	ZL 	Medium
		30	40	ZL	Medium
		48 110	<u>110</u> 120	ZL fS	Medium High
153	Т	0	40	ZL	Medium
155	'	40	<u>110</u>	ZL	Medium
		110	120	fS	High
154	Т	0	30	ZL	Medium
		30	45	ZL	Medium
		45	<u>110</u>	fS	High
		110	120	fS	High
156	Т	0	35	mZCL	Medium
		35 45	45	mZCL	Medium
		45 50	50 <u>80</u>	C C	Low Low
		50			
		80	120	С	low
157	Т	80 0		C mZCL	Low Medium

		40	45		Medium
		45	50		Low
		50 80	<u>80</u> 120		Low Low
158	Т	0	35	ZL	Medium
	·	35	45	ZL	Medium
		45	<u>80</u>		Medium
		80	120		Medium
159	Т	0	35	mSZL	High
		35 48	48 <u>80</u>		High Medium
		80	120		Medium
160	Т	0	35	ZL	Medium
		35	48	ZL	Medium
		48	<u>80</u>		Low
101	_	80	120	C ZL	Low
161	Т	0 38	38 45		Medium Medium
		45	55		Low
		55	<u>80</u>	fS	High
		80	120	fS	High
162	Т	0	38		Medium
		38 50	50 <u>90</u>		Medium
		90	90 120		High High
163	Т	0	38	ZL	Medium
		38	40	ZL	Medium
		40	58		Medium
		58	<u>90</u> 120	ZC ZC	Low
164	Т	90	38		Low Medium
104	'	38	<u>100</u>		High
		100	120	fS	High
165	Т	0	40		Medium
		40	45		Medium
		45 78	78 <u>90</u>		High Low
		90	120	C	Low
166	Т	0	35	ZL	Medium
		35	48		High
		48 80	<u>80</u> 120		Low
167	Т	0	40		Low Medium
107	,	40	70		Low
		70	<u>90</u>	ZL	Medium
		90	120		Medium
168	Т	0	35		Medium
		35 45	45 <u>90</u>	mZCL ZL	Medium Medium
		90	120		Medium
169	Т	0	20	ZL	Medium
		20	<u>75</u>		Medium
		75	120		Medium
170	Т	0 20	20 50		Medium Low
		50	50 <u>75</u>		Medium
		75			Medium
171	Т	0	33	ZL	Medium
		33	50	ZC	Low
		50 75	<u>90</u> 120		Medium Medium
172	Т	0	30		Medium
	·	30	40		Medium
		40	70		Medium
		70			Low
470	_	85 0	120 30		Low
173	Т	30	48		Medium Medium
		48	90		Medium
		90	120		Medium
174	Т	0	35		Medium
		35 40			Medium Medium
ı İ		40	60		Mediuili

I		60			Low
175	Т	85 0	120 35	ZC ZL	Low Medium
	·	35		fS	High
		68		С	Low
	_	90		C ZL	Low
176	Т	0 20	20 35	mZCL	Medium Medium
		35	<u>60</u>	С	Low
		60	120	С	Low
178	Т	0	28	ZL	Medium
		28 100		mZCL mZCL	Medium Medium
181	Т	0	28	ZL	Medium
		28		ZL	Medium
		50 80	<u>80</u> 120	ZL ZL	Medium Medium
182	Т	0	38	hZCL	Low
	·	38		hZCL	Low
		40		hZCL	Low
		50 80		fS fS	High
183	Т	0	30	hZCL	High Low
103	'	30			Low
		40	<u>70</u>	С	Low
		70		С	Low
184	Т	38	38 <u>60</u>	mSZL C	High Low
		60		С	Low
185	Т	0	38	mZCL	Medium
		38	<u>40</u>	mZCL	Medium
186	Т	40	120	C ZL	Low Medium
180	'	30		cSL	High
		45	<u>80</u>	С	Low
		80		С	Low
187	Т	0 28	28 45	mZCL C	Medium Low
		45		mZCL	Medium
		50	120	С	Low
188	Т	0	15	oZCL	Low
		15 60		hCL C	Low Low
		80		С	Low
192	Т	0	<u>40</u>	SCL	Medium
		40	120	C SCL	Low
193	Т	0 38		SCL	Medium Medium
		45		С	Low
194	Т	0	30	mCL	Medium
		30 45	45 <u>90</u>	mCL C	Medium
		90		С	Low Low
195	Т	0	30	SCL	Medium
		30		SCL	Medium
		50 90		SCL SCL	Medium Medium
196	Т	0	27	LmS	High
.55	<u> </u>	27	60	LmS	High
		60		LmS	High
40-	-	80	120 27	mS mSL	High
197	Т	27	50	LmS	High High
		50		LmS	High
		72		LmS	High
400	-	90	120	mS SCL	High Medium
198	Т	25	70	SCL	Medium
		<u>70</u>		SCL	Medium
199	Т	0	25	mCL	Medium
		25 55	55 80	mCL hCL	Medium Low
		80		hCL	Low

200	Т	0	25	mCL	Medium
		25	45	SCL	Medium
		45	55	SCL	Medium
		55	120	C/CL	Low
201	Т	0	25	mCL	Medium
		25	40	mCL	Medium
		40	120	С	Low
202	Т	0	25	mCL	Medium
		25	45	hCL	Low
		45	120	С	Low
203	Т	0	25	mSL	High
		25	47	LmS	High
		<u>47</u>	120	LmS	High
204	Т	0	40	LmS	High
Pit		40	120	LmS	High
205	Т	0	28	mCL	Medium
		28	65	С	Low
		65	120	С	Low
206	Т	0	32	SCL	Medium
		32	120	SCL	Medium
207	Т	0	28	SCL	Medium
		28	86	SCL	Medium
ļ		86	120	SCL	Medium
211	Т	0	28	mSL	High
		28 45	45 120	mSL mSL	High
		<u>45</u>	120		High
212	Т	0 17	17 27	mSL mSL	High
		17 <u>27</u>	120	mSL mSL	High High
242		0		mSL	High
213	Т	27	51	mSL	High
		51	60	LmS	High
		<u>60</u>		LmS	High
214	Т	0	30	SCL	Medium
214	'	30	50	SCL	Medium
		50	120	SCL	Medium
215	Т	0	28	mCL	Medium
			40	hCL	Low
		28	46	IICL	LOVV
		28 46	120	C	Low
238	Т				
238	Т	46	120	C SZL hCL	Low
238	Т	46	120 30 70	C SZL	Low High
238	T	46 0 30 <u>70</u> 0	120 30 70	C SZL hCL hCL mCL	Low High Low
		46 0 30 70 0 26	120 30 70 120 26 70	C SZL hCL hCL C	Low High Low Low Medium Low
		46 0 30 <u>70</u> 0 26 70	120 30 70 120 26	C SZL hCL hCL C hCL	Low High Low Low Low Medium Low Low
		46 0 30 70 0 26 70	120 30 70 120 26 70 120	C SZL hCL hCL C hCL mCL C hCL	Low High Low Low Medium Low Low Medium
239	Т	46 0 30 70 0 26 70 0	120 30 70 120 26 70 120 29	C SZL hCL hCL mCL C hCL	Low High Low Low Medium Low Low Medium Low Low Medium
239	Т	46 0 30 70 0 26 70 0 29 70	120 30 70 120 26 70 120 29 70	C SZL hCL hCL  mCL C hCL  mCL C	Low High Low Low Medium Low Low Medium Low Low Medium Low
239	Т	46 0 30 70 0 26 70 0 29 70	120 30 70 120 26 70 120 29 70 120	C SZL hCL hCL mCL C hCL C mCL C mCL	Low High Low Low Medium Low Low Medium Low Low Medium Low Low Medium
239	T	46 0 30 70 0 26 70 0 29 70	120 30 70 120 26 70 120 29 70 120 27	C SZL hCL hCL mCL C hCL C mCL C tSCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Medium
239 240 241	T	46 0 30 70 0 26 70 0 29 70 0 27 55	120 30 70 120 26 70 120 29 70 120 27 55	C SZL hCL hCL C hCL C mCL C tCL C C C	Low High Low Low Medium Low Low Medium Low Low Medium Low Low Medium Low
239	T	46 0 30 70 0 26 70 0 29 70 0 27 55	120 30 70 120 26 70 120 29 70 120 27 55 120 30	C SZL hCL hCL C hCL C mCL C mCL C mCL C mCL fSCL C	Low High Low Low Medium Low Low Medium Low Low Medium Low Low Medium Medium Medium Low
239 240 241	T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C	Low High Low Low Medium Low Low Medium Low Low Medium Low Medium Medium Medium Medium Medium
239 240 241 242	T T	46 0 30 70 0 26 70 0 29 70 0 27 55	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120	C SZL hCL hCL mCL C hCL  mCL C C mCL fSCL C fSCL C C C C	Low High Low Low Medium Low Low Medium Low Low Medium Low Medium Medium Low Medium Low
239 240 241	T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120 30	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C FSCL C C SCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Low Medium
239 240 241 242	T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 30	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120 30 58	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C FSCL C/CL SCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Low Medium
240 241 242 250	T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 30 58	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120 30 58 120	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C SCL SCL C C	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Medium Low Medium Low Medium Low
239 240 241 242	T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 30 58	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120 30 58 120 31	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C C mCL fSCL C/CL SCL C mCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Low Medium Medium Low Medium Medium Low Medium Medium Low Medium Medium Medium Medium Medium Medium
240 241 242 250	T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 30 58	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120 30 58 120 31 55	C SZL hCL hCL mCL C hCL mCL C mCL fSCL C mCL fSCL C/CL SCL SCL C mCL hCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Medium Low Medium Low Medium Low Medium Low Medium Low Medium Low
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 30 58	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C mCL fSCL C/CL SCL SCL C mCL hCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low
240 241 242 250	T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120 30 58 120 31 55 120	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C mCL fSCL C C mCL fSCL C C C C C C C C C C C C C C C C C C	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 29 60	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C mCL fSCL C/CL SCL SCL C mCL hCL SCL SCL SCL C mCL hCL SCL SCL SCL C mCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Low Medium Low
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55	120 30 70 120 26 70 120 29 70 120 27 55 120 30 60 120 30 58 120 31 55 120	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C mCL fSCL C C mCL fSCL C C C C C C C C C C C C C C C C C C	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Low Medium Medium Low Medium High High
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 29 60 75 120	C SZL hCL hCL mCL C hCL  mCL fSCL C mCL fSCL C mCL fSCL C/CL SCL SCL SCL C mCL hCL SCL L MCL L MCL MCL MCL MCL MCL MCL MCL M	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Low Medium Medium Low Medium High High High
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 29 60 75	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C C mCL fSCL C/CL SCL C mCL SCL SCL C mCL hCL SCL MCL hCL MCL hCL MCL MCL MCL MCL MCL MCL MCL MCL MCL M	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Medium Low Medium High High High Medium Medium High Medium
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75 0 0	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 29 60 75 120 33	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C C mCL fSCL C/CL SCL C mCL SCL SCL C MCL SCL SCL SCL SCL SCL SCL SCL SCL SCL S	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Medium Low Medium High High High Medium
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75 0 33 33	120 30 70 120 26 70 120 29 70 120 30 60 120 31 55 120 29 60 75 120 33 65	C SZL hCL hCL mCL C hCL mCL C C mCL fSCL C MCL fSCL C C MCL SCL SCL SCL SCL SCL SCL SCL SCL SCL S	Low High Low Low Medium Low Low Medium Low Medium Low Medium Low Medium Medium Low Medium Medium Low Medium High High High Medium Medium High High High
240 241 242 250 251	T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75 0 33 65	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 29 60 75 120 33 65 75	SZL hCL hCL mCL C hCL mCL fSCL C mCL fSCL C/CL SCL SCL C mCL hCL SCL SCL SCL SCL SCL SCL SCL SCL SCL S	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Medium Low Medium High High High Medium
240 241 242 250 251 257	T T T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75 0 33 65 75	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 29 60 75 120 33 65 75	C SZL hCL hCL mCL C hCL mCL fSCL C mCL fSCL C/CL SCL SCL C mCL hCL SCL SCL SCL SCL SCL MSL MSL MSL MSL	Low High Low Low Medium Low Low Medium Low Medium Medium Low Medium Medium Low Medium Medium Low Medium High High High High High High High
240 241 242 250 251 257	T T T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75 0 33 65 75	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 29 60 75 120 33 65 75 120	C SZL hCL hCL mCL C hCL  mCL fSCL C mCL fSCL C mCL SCL SCL SCL SCL SCL SCL SCL SCL MSL MSL MSL MSL MSL MCL	Low High Low Low Medium Low Low Medium Low Low Medium Medium Low Medium Medium Low Medium Medium Low Medium Medium Low Medium High High High High High High High High
240 241 242 250 251 257	T T T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75 0 33 65 75	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 31 55 120 33 65 75 120 33 65 75 120 345	C SZL hCL hCL mCL C hCL mCL fSCL C mCL fSCL C/CL SCL SCL C mCL hCL SCL SCL C mCL hCL SCL MSL MSL MSL MSL MSL MSL MCL MCL MCL MCL MCL MCL MCL MSL MSL MSL MSL MSL MSL MCL MCL	Low High Low Low Medium Low Low Medium Low Medium Medium Medium Medium Low Medium Medium Medium Low Medium Medium High High High High High High High High
240 241 242 250 251 257	T T T T T	46 0 30 70 0 26 70 0 29 70 0 27 55 0 30 60 0 31 55 0 29 60 75 0 33 45	120 30 70 120 26 70 120 29 70 120 30 60 120 30 58 120 31 55 120 31 55 120 33 65 75 120 25 45 65 120	SZL hCL hCL mCL C hCL mCL fSCL C mCL fSCL C mCL fSCL C mCL fSCL C mCL sCL SCL SCL SCL SCL SCL MSL MSL MSL MSL MSL MSL MSL MSL MSL MS	Low High Low Low Medium Low Low Medium Low Medium Medium Medium Medium Low Medium Medium High High High High High High High Medium High High Medium Medium Medium Medium Medium Medium High Medium

		28	40	hCL	Low
		40	54	hCL	Low
		54	75	fSCL	Medium
		75	120	С	Low
261	Т	0	27	mCL	Medium
		27	50	SCL	Medium
		50	70	mCL	Medium
		70	90	LmS	High
		90	120	LmS	High
262	Т	0	26	mCL	Medium
		26	45	SCL	Medium
		45	70	SC	Low
		70	120	hCL	Low
263	Т	0	28	mCL	Medium
		28	60	mCL	Medium
		60	92	hCL	Low
		92	120	С	Low
264	Т	0	26	mCL	Medium
		26	55	hCL	Low
		55	80	С	Low
		80	100	SCL	Medium
		<u>100</u>	120	SCL	Medium
265	Т	0	27	mCL	Medium
		27	40	hCL	Low
		40	50	С	Low
		50	70	hCL	Low
		70	120	С	Low
266	Т	0	30	mCL	Medium
		30	48	mCL	Medium
		48	120	C/CL	Low
267	Т	0	28	SCL	Medium
		28	52	LmS	High
		52	70	LmS	High
		<u>70</u>	120	Sandstone	N/A
268	Т	0	27	hCL	Low
		27	40	hCL	Low
		4.0	400	_	LOVA
		40	120	С	Low
269	Т	0	28	mCL	Medium
269	Т	0 28	28 45	mCL hCL	Medium Low
269	Т	0 28 45	28 45 55	mCL hCL C	Medium Low Low
269	Т	0 28 45 55	28 45	mCL hCL C C	Medium Low Low Low
269	T	0 28 45 55	28 45 55 120 30	mCL hCL C C	Medium Low Low Low Medium
		0 28 45 55 0 30	28 45 55 120 30 40	mCL hCL C C mCL	Medium Low Low Low Medium Medium
270	Т	0 28 45 55 0 30 40	28 45 55 120 30 <u>40</u> 120	mCL C C mCL mCL	Medium Low Low Low Medium Medium Low
		0 28 45 55 0 30 40	28 45 55 120 30 40 120	mCL C C mCL mCL C	Medium Low Low Medium Medium Low Medium Medium
270	Т	0 28 45 55 0 30 40 0	28 45 55 120 30 40 120	mCL C C mCL C mCL mCL mCL	Medium Low Low Medium Medium Low Medium Medium Medium Medium
270	Т	0 28 45 55 0 30 40 0 30	28 45 55 120 30 40 120 30 40	mCL C C mCL mCL C mCL mCL	Medium Low Low Medium Medium Low Medium Medium Medium Medium Medium
270	Т	0 28 45 55 0 30 40 0 30 40	28 45 55 120 30 40 120 30 40 45	mCL hCL C mCL mCL mCL mCL c	Medium Low Low Medium Medium Low Medium Medium Medium Medium Medium Medium Low
270 271	Т	0 28 45 55 0 30 40 0 30 40 45 60	28 45 55 120 30 40 120 30 45 60 120	mCL hCL C mCL mCL c mCL c C	Medium Low Low Medium Medium Low Medium Medium Medium Medium Medium Low Low
270	Т	0 28 45 55 0 30 40 0 30 40 45 60	28 45 55 120 30 40 120 30 40 45 60 120	mCL hCL C mCL mCL mCL mCL C sCL	Medium Low Low Medium Medium Low Medium
270 271	Т	0 28 45 55 0 30 40 0 30 40 45 60	28 45 55 120 30 40 120 30 40 45 60 120 40 45	mCL hCL C C mCL mCL C C C C SCL SCL	Medium Low Low Medium Medium Low Medium Medium Medium Medium Medium Low Low Medium Medium Medium
270 271	Т	0 28 45 55 0 30 40 0 30 40 45 60	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55	mCL hCL C C mCL mCL c mCL C C SCL SCL C	Medium Low Low Medium Medium Low Medium Medium Medium Medium Medium Medium Low Medium Low Low Medium Medium Low
270 271	Т	0 28 45 55 0 30 40 0 30 45 60 0 45 55	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55	mCL hCL C C mCL mCL mCL c sCL C C C C	Medium Low Low Medium Medium Low Medium Medium Medium Medium Low Low Medium Low Low Low Medium Low Low
270 271 272	T	0 28 45 55 0 30 40 0 30 40 45 60 45 55 100	28 45 55 120 30 40 120 30 45 60 120 40 45 55 100 120	mCL hCL C mCL mCL mCL c sCL C C C C	Medium Low Low Medium Medium Low Medium Medium Medium Medium Low Low Medium Low Low Low Medium Low Low
270 271	Т	0 28 45 55 0 30 40 0 30 40 45 60 0 45 55 100	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55 100 120	mCL hCL C C mCL mCL mCL C C SCL SCL C C C mCL	Medium Low Low Medium Medium Low Medium Medium Medium Medium Low Low Medium Low Low Medium
270 271 272	T	0 28 45 55 0 30 40 40 45 60 0 40 45 55 100	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55 100 120 35 40	mCL hCL C C mCL mCL C C SCL SCL C C C mCL mCL	Medium Low Low Medium Medium Low Medium Medium Medium Medium Low Low Medium Low Low Medium
270 271 272 273	T	0 28 45 55 0 30 40 0 30 40 45 60 0 45 55 100 0 35 40	28 45 55 120 30 40 120 30 45 60 120 40 45 55 100 120 35 40 120	mCL hCL C C mCL mCL C C C C C C C C C C C C C	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Medium Low Low Low Low Low Low Low Medium Low Low
270 271 272	T	0 28 45 55 0 30 40 0 30 40 45 60 0 40 45 55 100 0 35 40	28 45 55 120 30 40 120 30 45 60 120 40 45 55 100 120 35 40 120	mCL hCL C C mCL mCL C C C C C C C C C SCL SCL C C C SCL SCL	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Low Medium Medium Low Low Medium Low Low Low Low Medium Low Low Medium
270 271 272 273	T	0 28 45 55 0 30 40 0 30 40 45 60 0 45 55 100 0 35 40	28 45 55 120 30 40 120 30 45 60 120 40 45 55 100 120 35 40 120 35 40	mCL hCL C C mCL mCL mCL C C C C SCL SCL C C SCL SCL C SCL SCL	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Medium Medium Medium Low Low Medium Low Low Medium
270 271 272 273	T	0 28 45 55 0 30 40 0 30 40 45 60 0 45 55 100 0 35 40	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55 100 120 35 40 120 35 40 50	mCL hCL C C mCL mCL mCL c C mCL mCL c C SCL SCL C C SCL SCL SCL SCL SCL SCL S	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Low Low Medium Low Low Medium Low Low Medium
270 271 272 273	T	0 28 45 55 0 30 40 0 30 40 45 60 0 45 55 100 0 35 40	28 45 55 120 30 40 120 30 45 60 120 40 45 55 100 120 35 40 120 35 40	mCL hCL C C mCL mCL mCL C C C C SCL SCL C C SCL SCL C SCL SCL	Medium Low Low Medium Medium Medium Medium Medium Medium Low Medium Low Low Medium Medium Low Low Medium
270 271 272 273	T T	0 28 45 55 0 30 40 0 30 40 45 60 0 45 55 100 0 35 40 0 35 40	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55 100 120 35 40 120 35 40 50 70 120	mCL hCL C C mCL mCL mCL C C SCL SCL C SCL SCL SCL SCL SCL SCL	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Medium Low Low Medium Medium Low Medium Medium Low
270 271 272 273	T	0 28 45 55 0 30 40 0 30 40 45 60 0 40 45 55 100 0 35 40 0 35 40	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55 100 120 35 40 120 35 40 120 35 35 35 30 30 30	mCL hCL C C mCL mCL C C C C C SCL SCL C C C SCL SCL C C C MCL C C MCL MCL	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Low Low Medium Low Low Medium Low Low Medium Medium Low Low Medium Medium Medium Low Medium
270 271 272 273	T T	0 28 45 55 0 0 30 40 40 45 60 0 35 40 50 70 0 30 30 30 30	28 45 55 120 30 40 120 30 40 45 55 100 120 35 40 120 35 40 120 35 40 120 35 40 50 120 30 45	mCL         hCL           c         c           mCL         mCL           mCL         mCL           mCL         c           scl         scl           scl	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Medium Low Medium
270 271 272 273	T T	0 28 45 55 0 0 30 40 45 60 0 35 40 0 35 40 50 70 0 30 45	28 45 55 120 30 40 120 30 40 45 60 120 40 45 55 100 120 35 40 120 35 40 120 35 40 50 70 120 30 45 75	mCL hCL C C mCL mCL mCL C C SCL SCL C C C SCL SCL C C C mCL mCL hCL C SCL SCL SCL SCL SCL SCL SCL SCL SCL	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Low Medium Low Low Medium Medium Low Low Medium Medium Low Medium Low
270 271 272 273	T T	0 28 45 55 0 0 30 40 40 45 60 0 35 40 50 70 0 30 30 30 30	28 45 55 120 30 40 120 30 40 45 55 100 120 35 40 120 35 40 120 35 40 120 35 40 50 120 30 45	mCL         hCL           c         c           mCL         mCL           mCL         mCL           mCL         c           scl         scl           scl	Medium Low Low Medium Medium Low Medium Medium Medium Low Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Medium Medium Low Medium Medium Medium Low Medium Medium Medium Medium Medium Medium Medium Medium Medium Low Medium Medium Low Medium Low Medium Low Medium Low Medium Low
270 271 272 273 274	T T T	0 28 45 55 0 0 30 40 40 45 60 0 35 40 50 70 0 30 45 75 85	28 45 55 120 30 40 120 30 40 45 55 100 120 35 40 120 35 40 120 35 40 120 35 40 50 70 120 30 45 75	mCL         hCL           hCL         c           mCL         mCL           mCL         mCL           mCL         mCL           scl         scl           scl	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Medium Low Medium Low Medium Medium Low Medium Medium Low Medium Low Medium Medium Low Low Low Low Low Low
270 271 272 273	T T	0 28 45 55 0 0 30 40 40 45 55 100 0 35 40 50 70 0 30 45 75 85 0 0	28 45 55 120 30 40 120 30 40 45 55 100 120 35 40 120 35 40 120 35 40 120 35 40 50 70 120 30 45 75 85	mCL         hCL           hCL         c           mCL         mCL           mCL         mCL           mCL         c           scl         scl           scl	Medium Low Low Medium Medium Medium Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Low Medium Medium Low Medium
270 271 272 273 274	T T T	0 28 45 55 0 0 30 40 40 45 60 0 35 40 50 70 0 30 45 75 85	28 45 55 120 30 40 120 30 40 45 55 100 120 35 40 120 35 40 120 35 40 120 35 40 50 70 120 30 45 75 85 120	mCL         hCL           hCL         c           mCL         mCL           mCL         mCL           mCL         c           scl         scl           scl	Medium Low Low Medium Medium Low Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Low Medium Medium Low Medium Low Medium Medium Low Medium Medium Low Medium Low Medium Low Medium Low Low Low Low Low
270 271 272 273 274	T T T	0 28 45 55 0 0 30 40 40 45 60 100 0 35 40 50 70 0 30 45 75 85 0 0 35 45 75 85 0 0 35	28 45 55 120 30 40 120 30 40 45 55 100 120 35 40 120 35 40 120 35 40 120 36 40 40 45 40 45 40 40 45 40 40 40 40 40 40 40 40 40 40 40 40 40	mCL         hCL           hCL         c           mCL         mCL           mCL         mCL           mCL         c           scl         scl           scl	Medium Low Low Medium Medium Medium Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Low Medium
270 271 272 273 274	T T T	0 28 45 55 0 0 30 40 40 45 60 0 35 40 50 70 0 30 45 75 85 0 0 35 48	28 45 55 120 30 40 120 30 40 45 60 120 35 40 120 35 40 120 35 40 50 70 120 36 45 75 85 120 36 48 90	mCL       hCL         hCL       C         mCL       mCL         mCL       mCL         mCL       C         sCL       sCL         sCL       sCL </th <th>Medium Low Low Medium Medium Medium Medium Low Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Low Medium Low Medium Low Medium Low Medium Low Low Low Low Low Low Low Low Low Low</th>	Medium Low Low Medium Medium Medium Medium Low Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Medium Low Medium Low Medium Low Medium Low Medium Low
270 271 272 273 274 276	T T T	0 28 45 55 0 0 30 40 40 45 55 100 0 35 40 50 70 0 30 45 75 85 0 0 35 48 90	28 45 55 120 30 40 120 30 40 45 60 120 35 40 120 35 40 120 35 40 120 35 40 120 35 40 120 35 40 120 36 40 120 37 40 40 40 41 41 40 40 41 40 40 40 40 40 40 40 40 40 40 40 40 40	mCL         hCL           hCL         c           mCL         mCL           mCL         mCL           mCL         c           scl         scl           scl	Medium Low Low Medium Medium Medium Medium Medium Medium Low Low Medium Medium Low Low Medium Medium Low Low Medium Low Medium Medium Low Medium Low Medium Low Medium Low

				_	_
		35	55		Low
		55	70	С	Low
		70 90		C C	Low
070	-	0		mCL	Low
279	Т	35	55	mCL	Medium Medium
		55	<u>80</u>	С	Low
		80		С	Low
280	Т	0	40	SCL	Medium
		40	<u>50</u>	С	Low
		50	120	С	Low
281	Т	0	38	mCL	Medium
		38	40	hCL	Low
		40		hCL	Low
		55	<u>70</u>	С	Low
		70		С	Low
282	Т	0	<u>30</u>	mCL mCL	Medium
		30 40	40 120	C	Medium Low
283	Т	0	30	mCL	Medium
203	'	30	<u>40</u>	mCL	Medium
		40		С	Low
284	Т	0	35	mCL	Medium
		35	60	hCL	Low
		60	80	С	Low
		80	120	С	Low
285	Т	0	35	mCL	Medium
		35	55	hCL	Low
		55	<u>70</u>	С	Low
		70	120	С	LOW
286	Т	0	35	mCL mCL	Medium
		35 45	45 55	hCL	Medium Low
		55	<u>100</u>	C	Low
		100		С	Low
287	Т	0	35	mSL	High
		35	75	mSL	High
		55	<u>95</u>	LmS	High
		95	120	LmS	High
288	Т	0	35	mCL	Medium
		35	45	mCL	Medium
		45	50	SCL	Medium
		50 60		C C	Low Low
289	Т	0	39	SCL	Medium
203	'	39	<u>40</u>	SCL	Medium
		40		С	Low
290	Т	0	35	mCL	Medium
		35	<u>70</u>	С	Low
		70	120	С	Low
291	Т	0	38	mCL	Medium
		38		hCL	Low
		40		С	Low
		80	120	C	Low
292	Т	0 40	<u>40</u> 120	SCL C	Medium Low
202	<b>-</b>	0	39	SCL	Medium
293	Т	39	40	hCL	Low
		40		C	Low
294	Т	0		SCL	Medium
_3.	,	40		SCL	Medium
		45	120	С	Low